



香港大學

THE UNIVERSITY OF HONG KONG

# Application-Oriented Stability, Reliability, and Robustness of GaN Power Devices

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2025/08/14

# Research scope of my group

## Performance, Reliability, Cost

### Sciences

### Applications

Physics  
& Material

Device  
Design

Processing  
Technologies

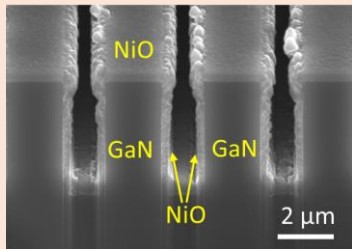
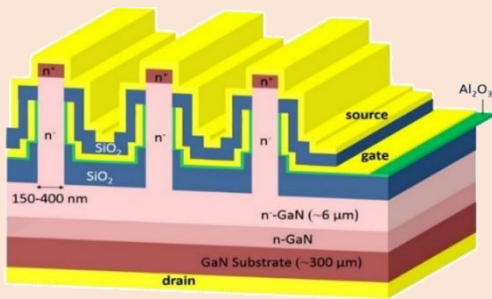
Device Charact.  
and Application

Robustness  
& Reliability

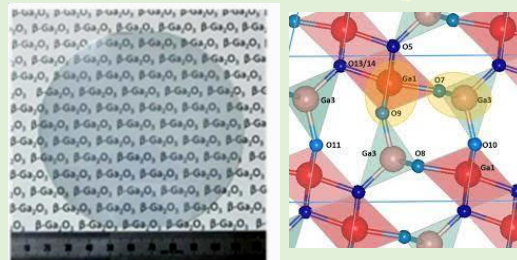
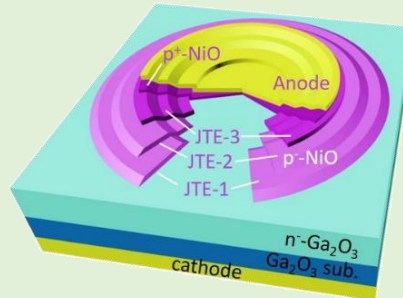
Packaging

Converter

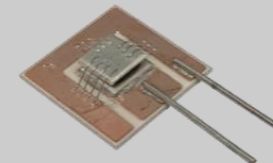
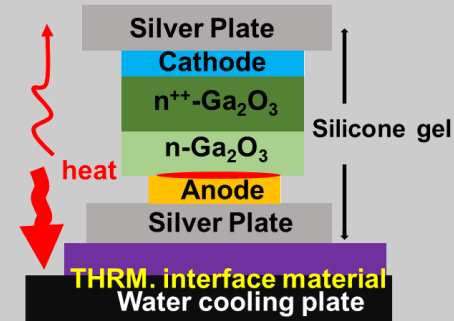
### Multidimensional Device Architectures



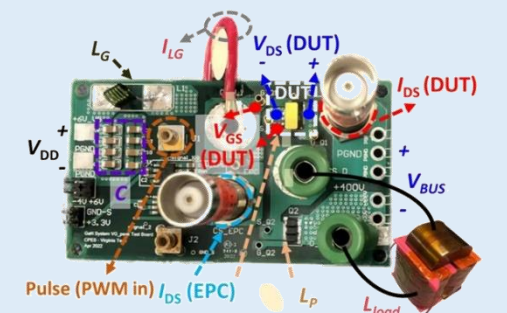
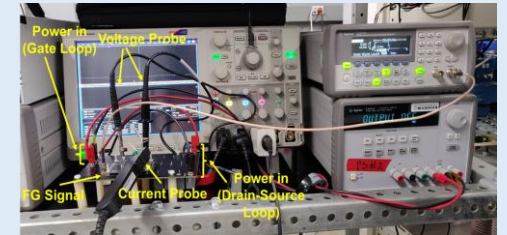
### (Ultra) Wide Bandgap Materials



### Packaging & Thermal Management



### Circuit-based Reliability & Application



we work on Si IGBT, SiC MOSFET, GaN HEMT, Ga<sub>2</sub>O<sub>3</sub> devices...

# Power semiconductors as pathways to carbon neutrality

**nature reviews** electrical engineering

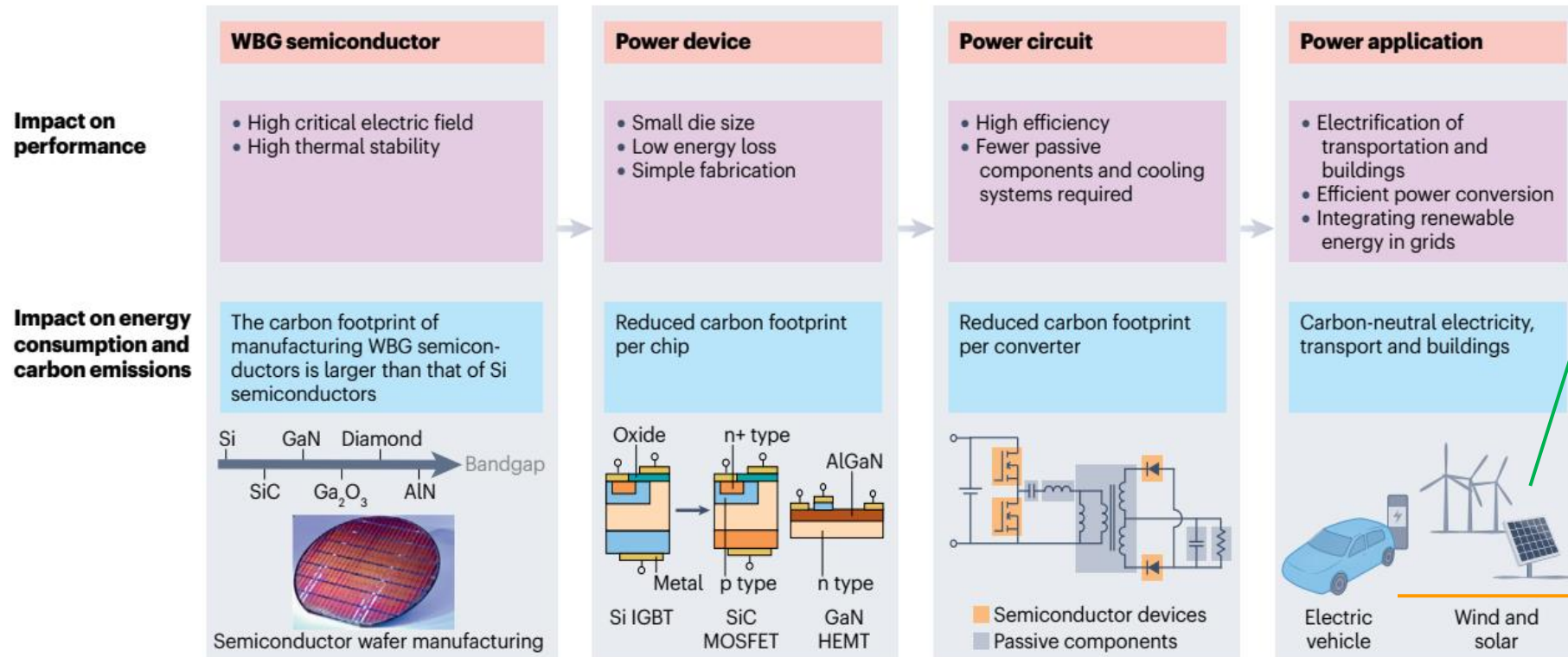
Review Article | Published: 21 January 2025

## Wide-bandgap semiconductors and power electronics as pathways to carbon neutrality

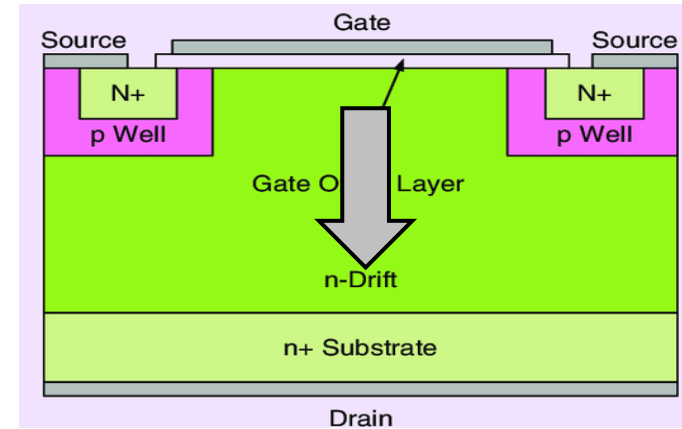
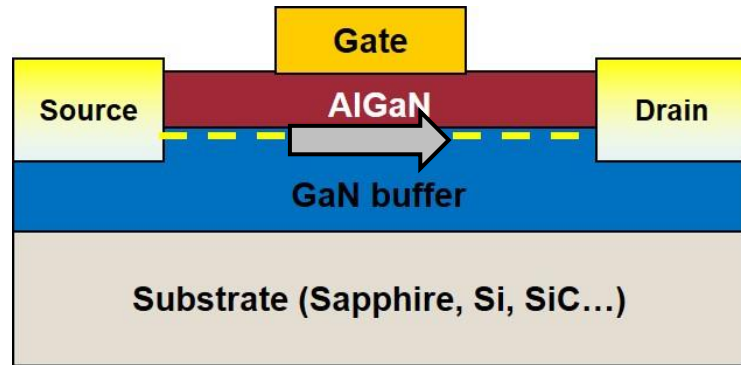
Yuhao Zhang , Dong Dong , Qiang Li , Richard Zhang, Florin Udrea & Han Wang 

*Nature Reviews Electrical Engineering* **2**, 155–172 (2025) | [Cite this article](#)

WBG replacing Si can enable an annual carbon saving of at least 20 million tonnes in the USA – annual emissions of 4 million gasoline passenger vehicles

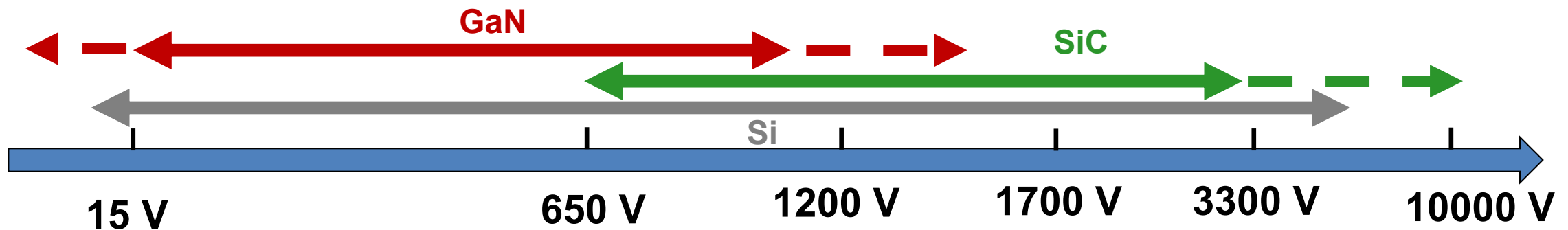


# WBG Devices: GaN HEMTs and SiC MOSFETs (>\$3 billion market)

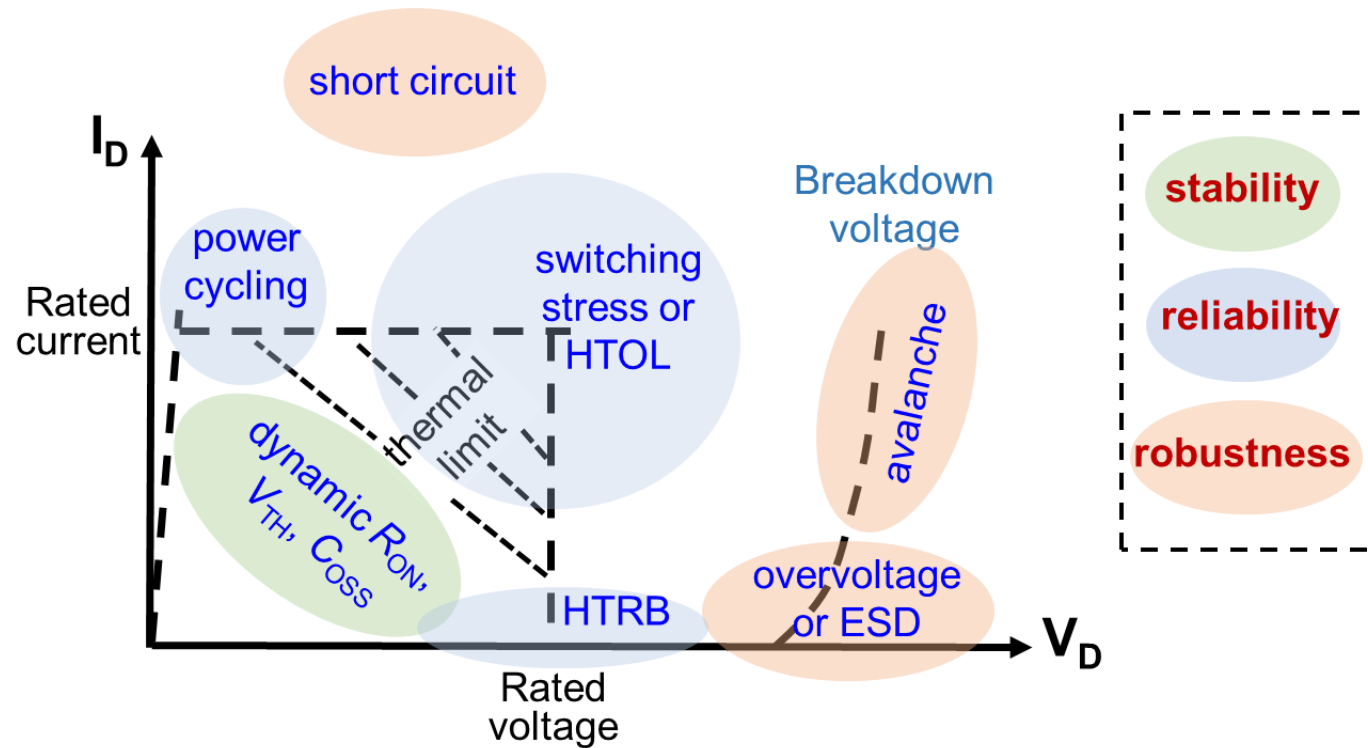


- ✓ 2DEG: mobility  $>1500 \text{ cm}^2/\text{Vs}$
- ✓ easy for IC integration
- ✗ large chip size for high-voltage
- ✗ thermal and E-field management
- ✗ robustness (avalanche and short-circuit)

- ✗ MOS: mobility  $\sim 100 \text{ cm}^2/\text{Vs}$
- ✗ Mostly discrete
- ✓ high current
- ✓ small chip size for high-voltage
- ✓ easier thermal management



# Stability, reliability, and robustness – framework



J. Kozak *et al.*, “Stability, reliability, and robustness of GaN power devices: a review,” IEEE Trans. Power Electron., 2023

## Why GaN is special?

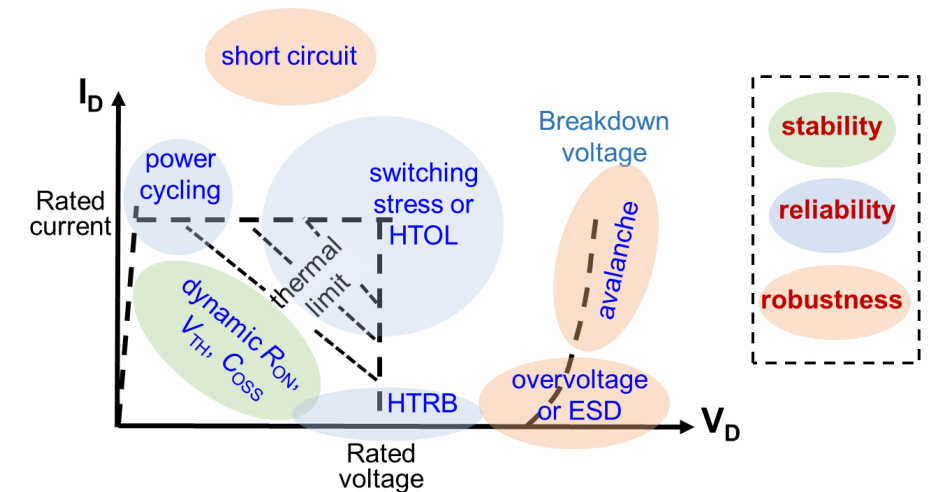
- Dynamic stability
  - Dynamic  $R_{ON}$ : conduction loss
  - Hysteresis  $C_{OSS}$  loss: high-frequency switching loss
- Overvoltage and surge energy robustness
  - No avalanche capability
- Short circuit robustness
- Gate reliability and robustness
- **Must be characterized under inductive switching conditions**





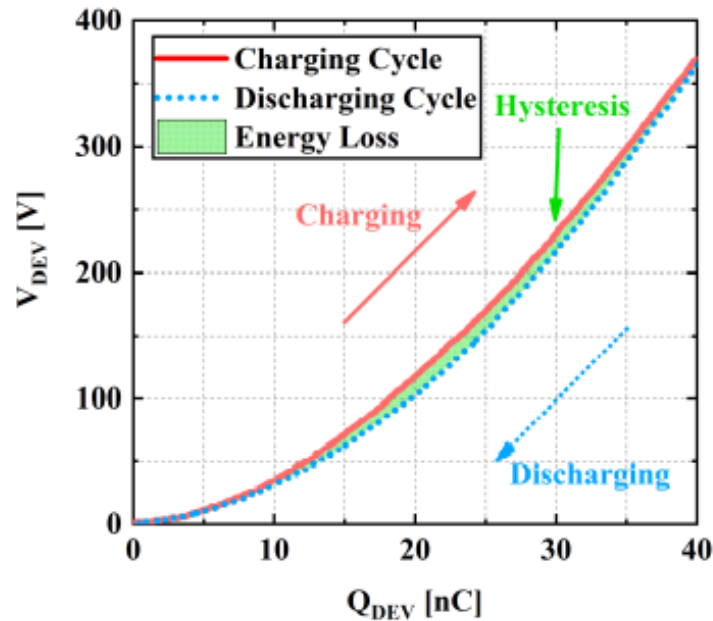
# Outline

- **Lateral GaN HEMT Reliability**
  - Output capacitance loss
  - Overvoltage robustness and lifetime
  - Gate reliability and lifetime
- **Bidirectional GaN**
- **Vertical GaN Devices: Performance and Reliability**
  - Dynamic  $R_{ON}$ , avalanche, short-circuit
  - MHz converter application
- **Summary**

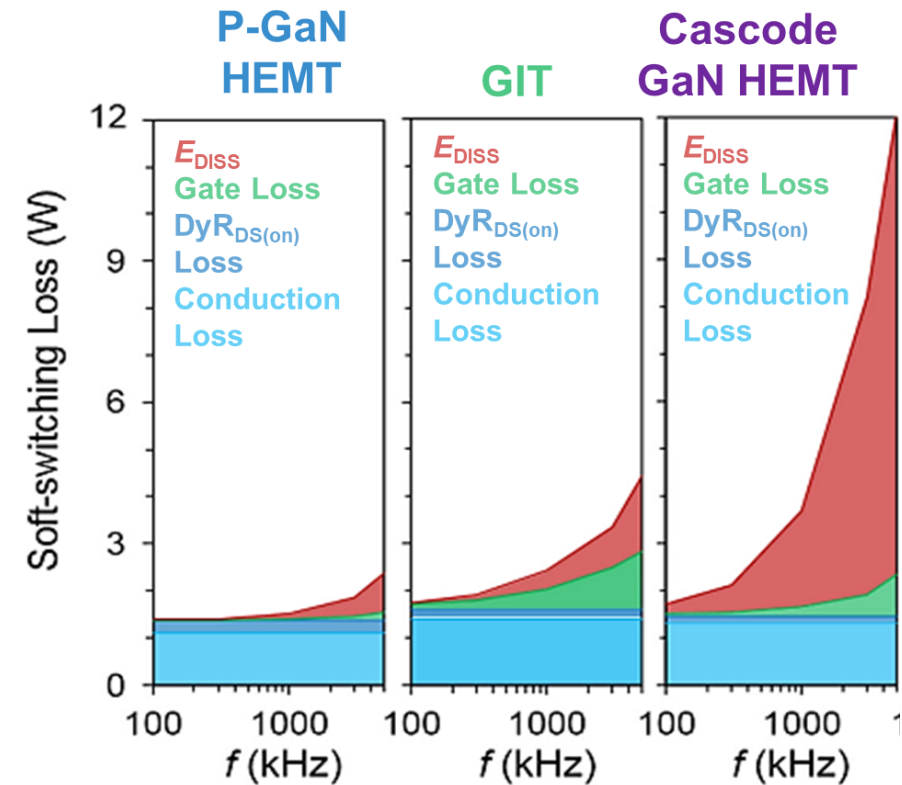


# Hysteresis $C_{OSS}$ loss

- $C_{OSS}$  loss: generated when  $C_{OSS}$  is charged and discharged in OFF-state (an ideal lossless process)
- “Hysteresis Loss” : energy stored in  $C_{OSS} \neq$  energy discharged from  $C_{OSS}$



- A potential issue for GaN HEMTs, especially at (very) high-frequencies soft-switching applications, i.e., at MHz level.

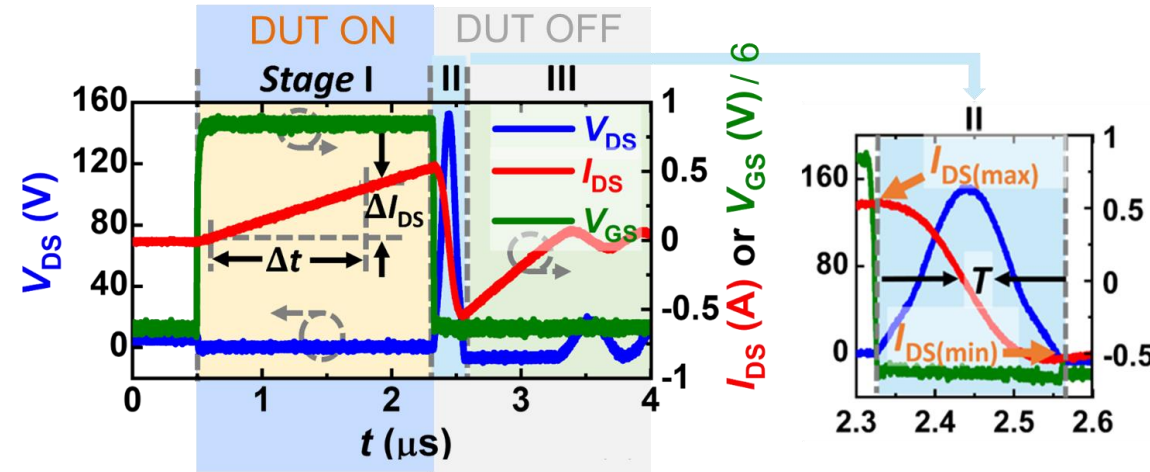
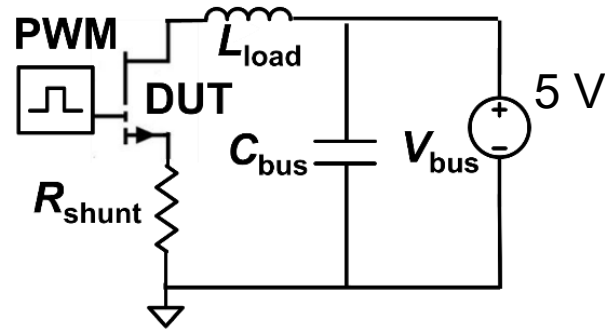


G. Zulauf *et al.*, IEEE Trans. on Power Electron., 2018.

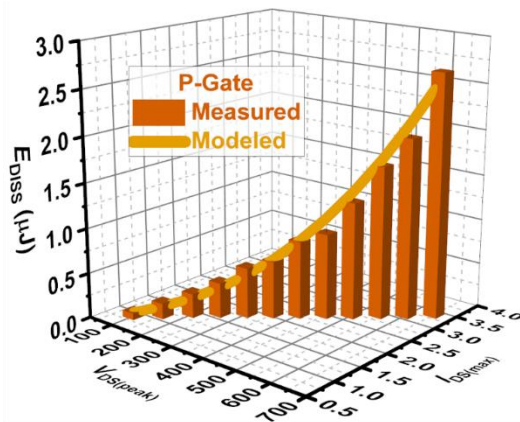
A. Jafari *et al.*, IEEE Trans. on Power Electron., 2020.



# $C_{OSS}$ loss characterization and modeling – discrete GaN



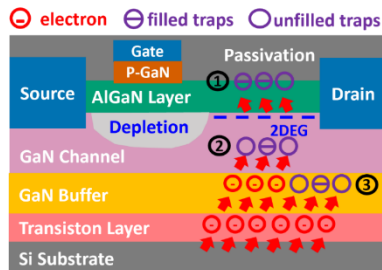
- $L_{load}$  resonates with DUT's  $C_{OSS}$
- Minimal turn-off loss
- $C_{OSS}$  loss extracted from the resonance



$$P_{OSS} = f_{sw} k [\alpha + \beta I_{DS(max)}] V_{DS(peak)}^\gamma$$

$f_R$	DUT	$k$	$\alpha$	$\beta$	$\gamma$
2 MHz	P-gate	$1.45 \times 10^{-11}$	0.42	0.33	1.86
	HD-GIT	$0.95 \times 10^{-16}$	0.54	0.37	3.42
	Direct-drive	$4.12 \times 10^{-10}$	0.03	0.30	1.20
6.78 MHz	P-Gate	$1.81 \times 10^{-11}$	0.36	0.18	1.84
	HD-GIT	$2.51 \times 10^{-15}$	0.29	0.22	3.32
	Direct-drive	$2.58 \times 10^{-11}$	0.01	0.20	1.69

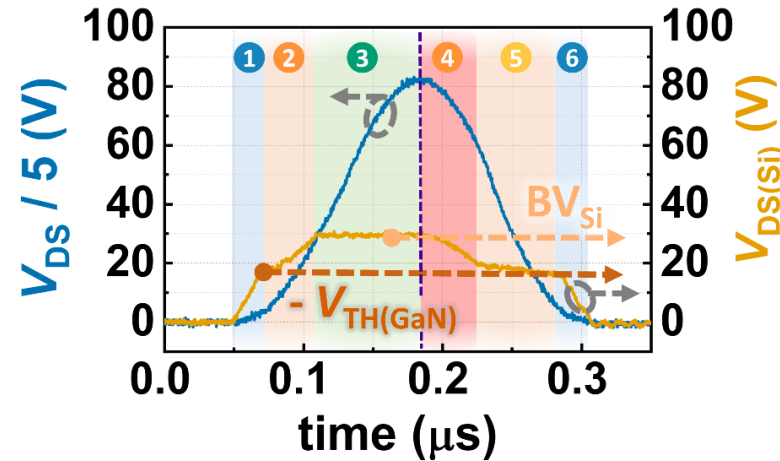
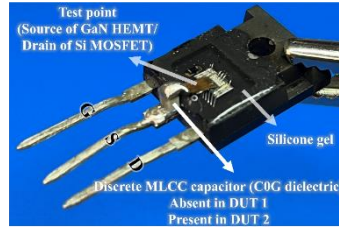
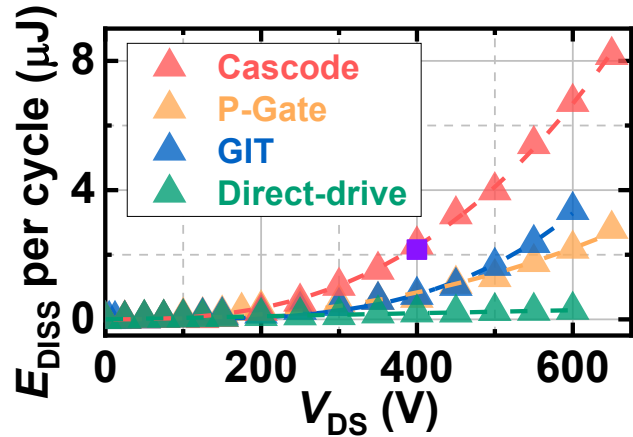
- $E_{DISS}$  dependent on resonance frequency (dv/dt), voltage (power law), and current (linear), weak dependence on  $T$
- Related to fast traps, with de-trapping time constants distinct from dynamic  $R_{on}$



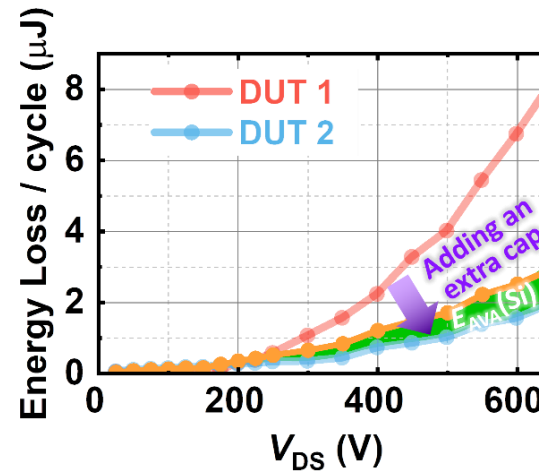
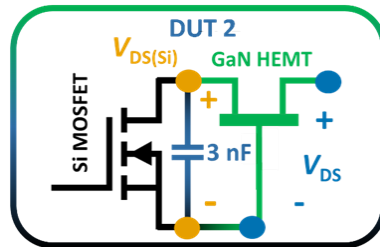
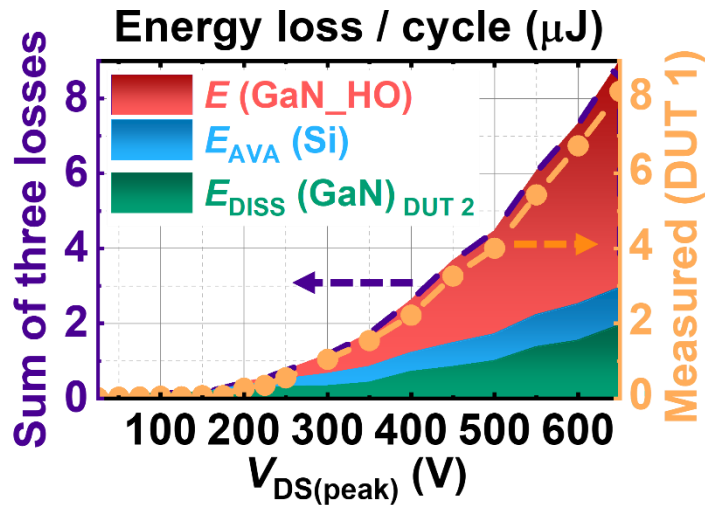
Q. Song *et al.*, "Output Capacitance Loss of GaN HEMTs in Steady-State Switching," IEEE Trans. on Power Electron., 2023.



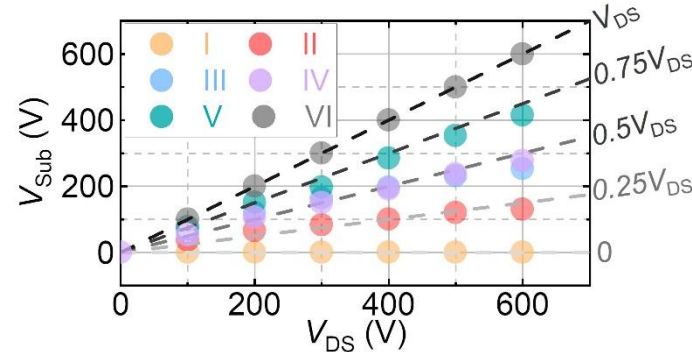
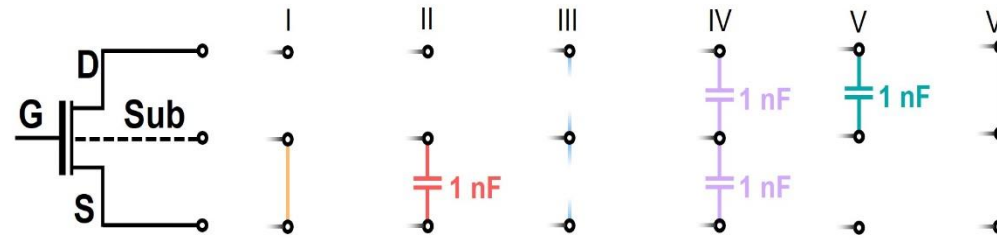
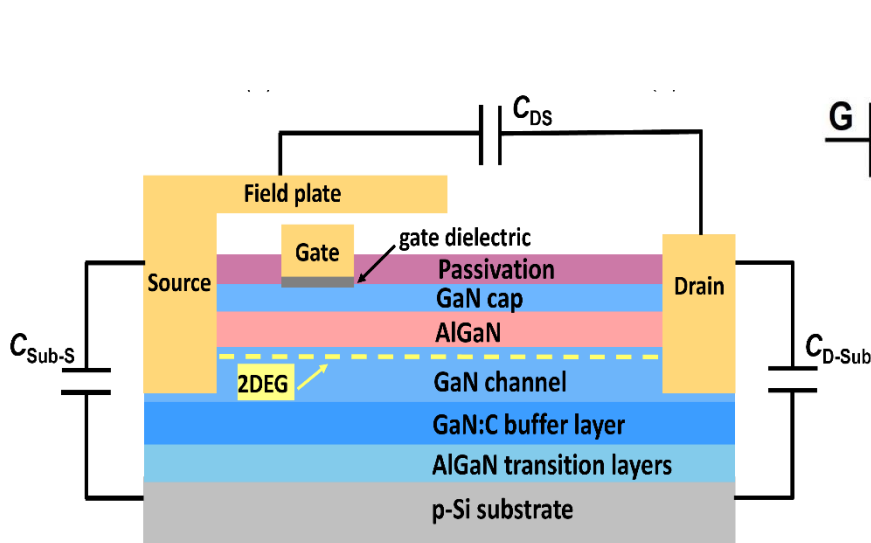
# Higher $C_{OSS}$ loss in GaN Cacode: two additional origins



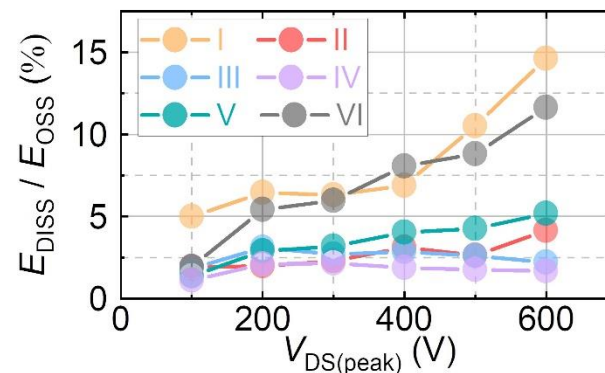
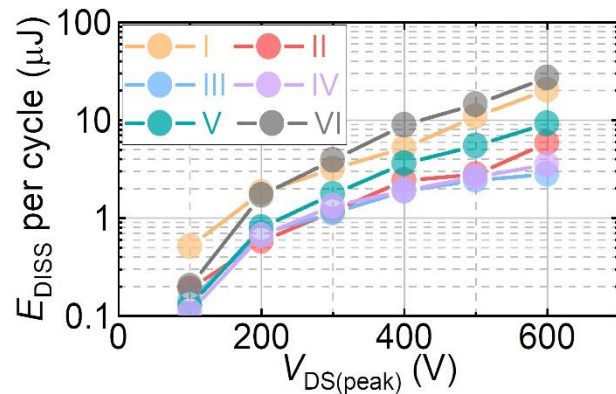
- $C_{OSS}$  loss much higher in GaN cascode devices
- #1:  $C_{OSS}$  loss in GaN HEMT
- #2: Si avalanche loss
- #3: GaN hard turn-on loss (could be dominant)
- #2 and #3 are both due to Si avalanche in GaN cascode
- Solution: increasing Si  $C_{OSS}$  to make an avalanche-free cascode -> 75% less loss in soft switching



# Minimizing intrinsic $C_{OSS}$ loss in GaN HEMT



- $C_{OSS}$  loss of GaN-on-Si HEMT can be reduced by tuning the substrate bias ( $V_{SUB}$ ) in dynamic switching
- Compared to sub-source-shorting, at  $V_{SUB} = 0.5V_{DS}$ ,  $E_{DISS}$  reduced by up to 86%,  $E_{DISS}/E_{OSS}$  ratio decreased from 14.6% to 2.2%
- Physics related to depletion front profile at different  $V_{SUB}$



Q. Song *et al.*, "Minimizing Output Capacitance Loss in GaN Power HEMT," IEEE Trans. on Power Electron., 2024.



# Outline

- **Lateral GaN HEMT Reliability**

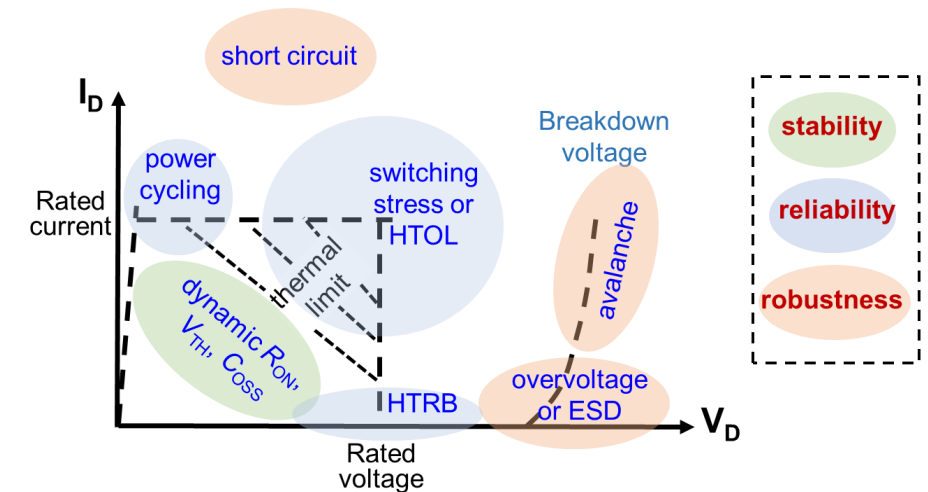
- Output capacitance loss
- Overvoltage robustness and lifetime
- Gate reliability and lifetime

- **Bidirectional GaN**

- **Vertical GaN Devices: Performance and Reliability**

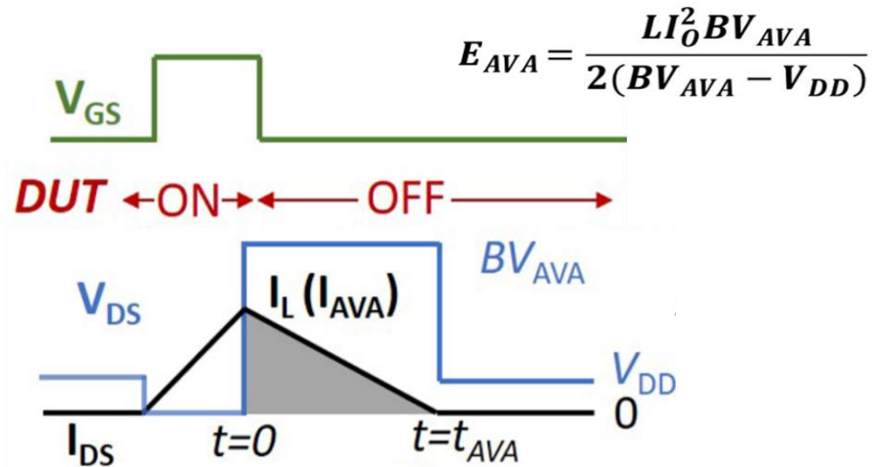
- Dynamic  $R_{ON}$ , avalanche, short-circuit
- MHz converter application

- **Summary**

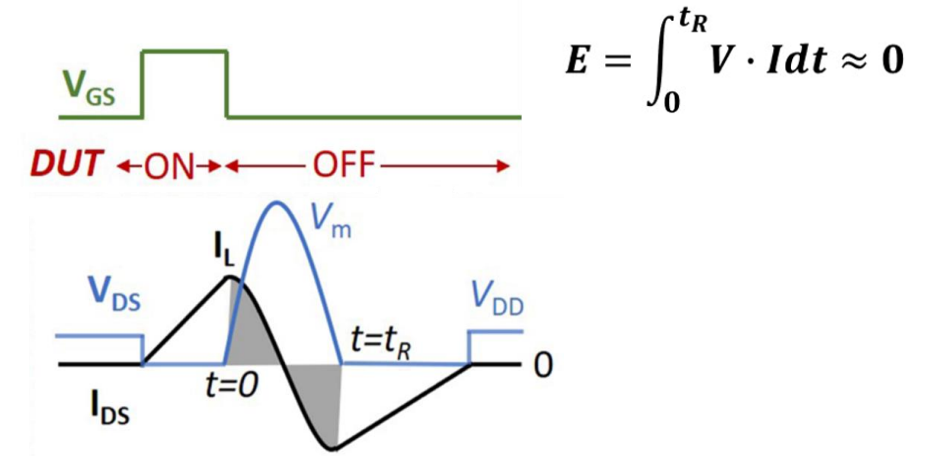


# Surge-energy robustness: Si/SiC MOSFETs v.s. GaN HEMTs

## Si & SiC MOSFET:



## GaN HEMT:



Withstand process

avalanching

LC resonance & reverse conduction

Energy path

dissipation in device in  
avalanching

little/no dissipation in withstand;  
dissipation in reverse conduction

Limiting factor

avalanche energy

overvoltage capability

Failure mechanism

thermal run-away

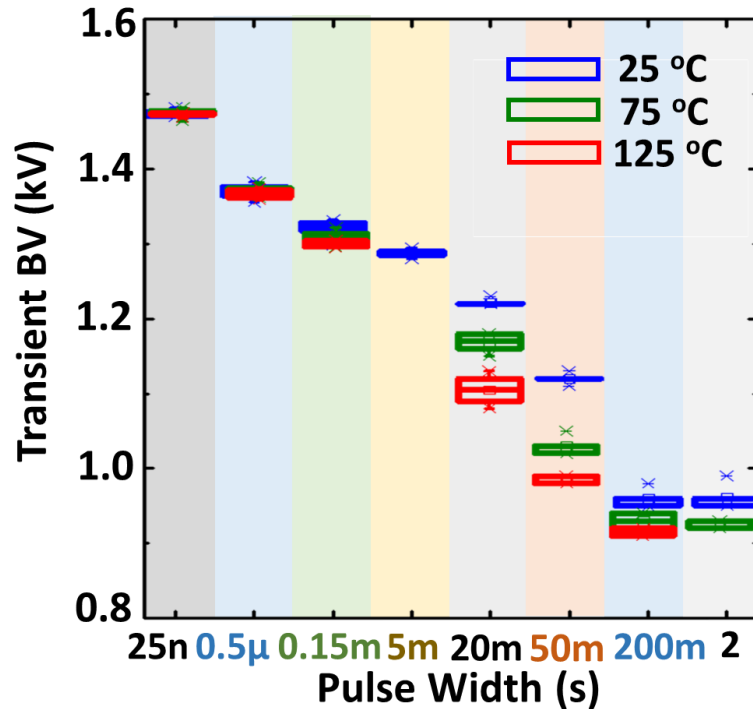
E-field induced breakdown

R. Zhang *et al.*, "Surge energy and overvoltage ruggedness of p-gate GaN HEMTs", IEEE Trans. Power Electron., 2020



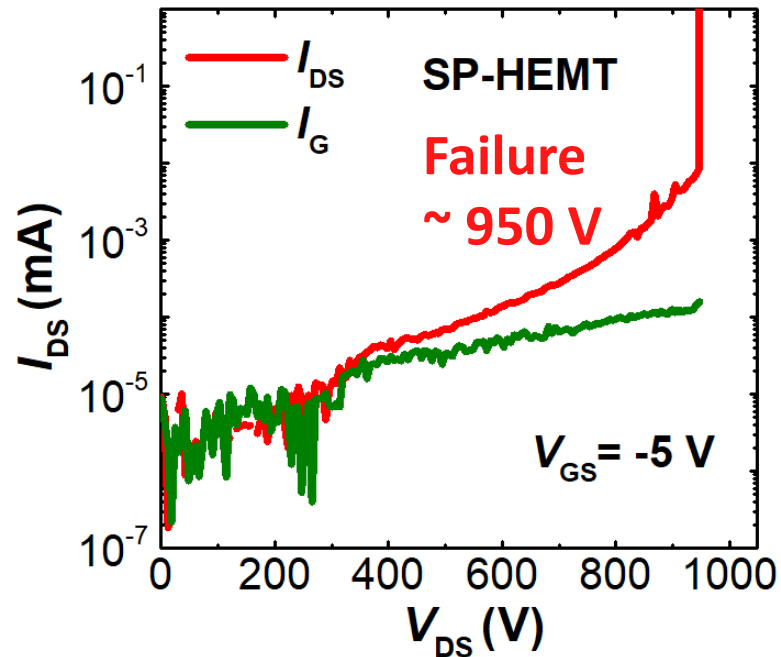
# Dynamic breakdown voltage

## Inductive Switching Circuit



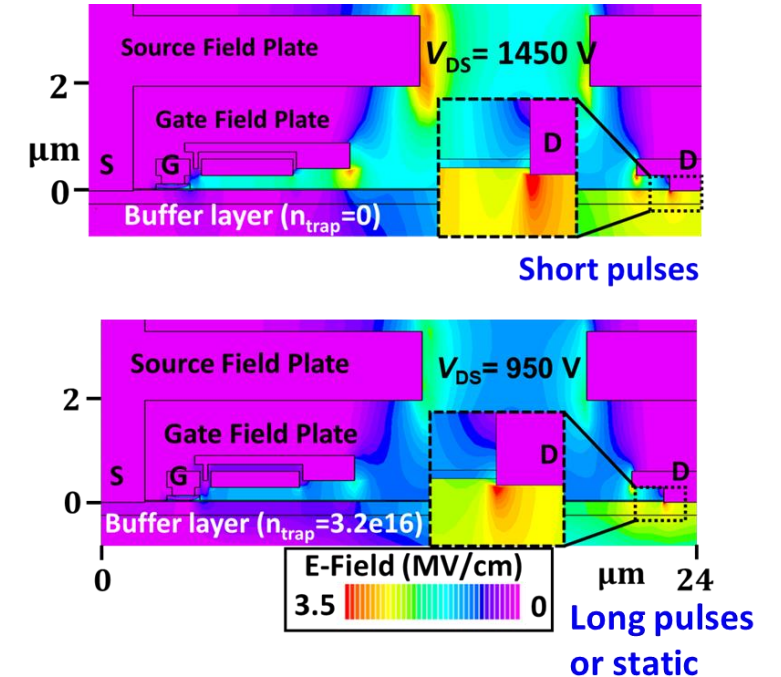
- BV reduce with pulse width

## Quasi-static I-V sweep



- BV converges to 'static' BV when PW > 200 ms
- Dynamic BV > Static BV

## Physical mechanism

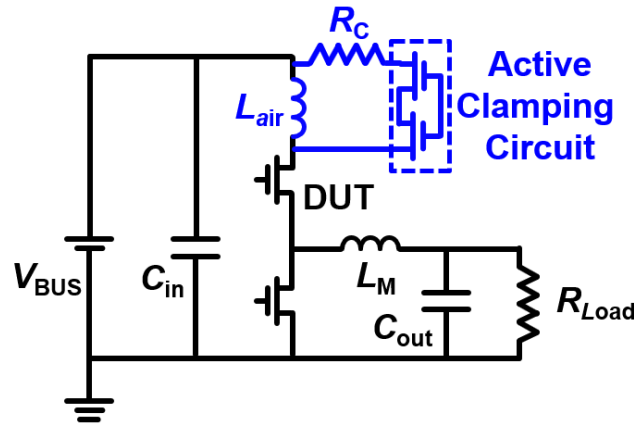


- Time-dependent buffer trapping
- Impact peak E-field

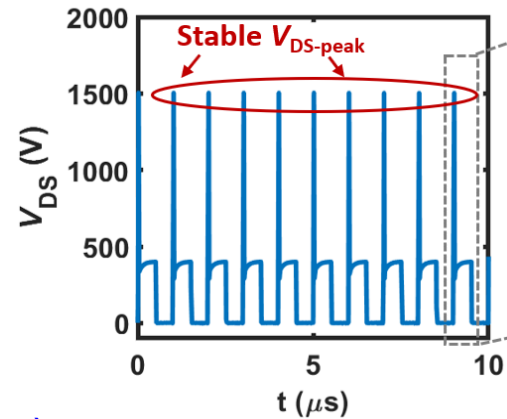
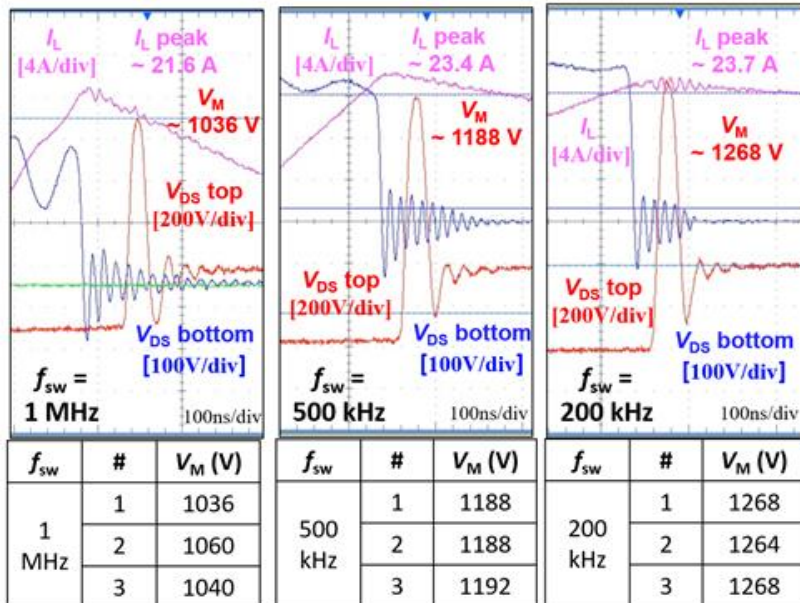
R. Zhang *et al.*, "Dynamic breakdown voltage of GaN power HEMTs", IEDM, 23.3, 2020



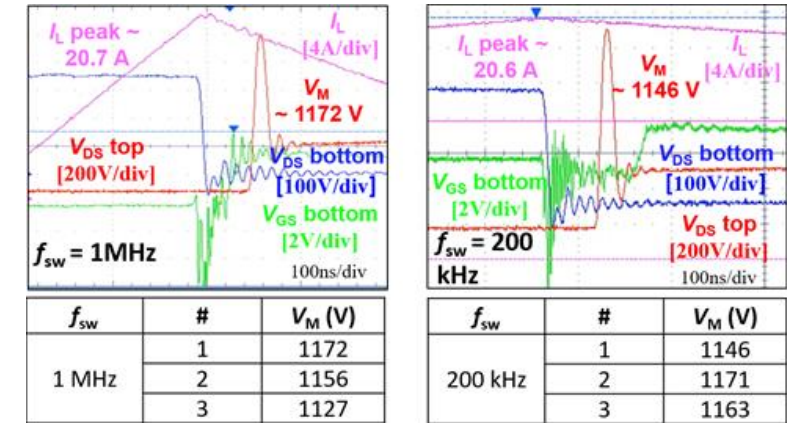
# Overvoltage switching at high frequency up to Megahertz



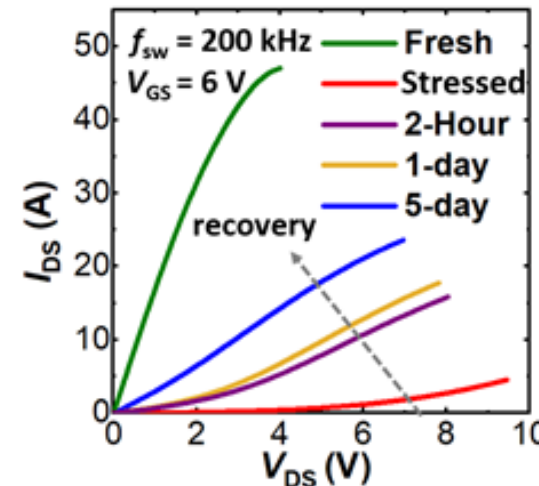
SP-HEMT (BV drop at higher  $f_{sw}$ )



## HD-GIT



## Repetitive UIS @ 75% BV



- Overvoltage switching at high  $f_{sw}$  triggers a new failure mechanism: thermal failure due to significant dynamic  $R_{ON}$  increase
- Qualification method: repetitive UIS
- Dynamic  $R_{ON}$ : the true limiter for overvoltage lifetime?

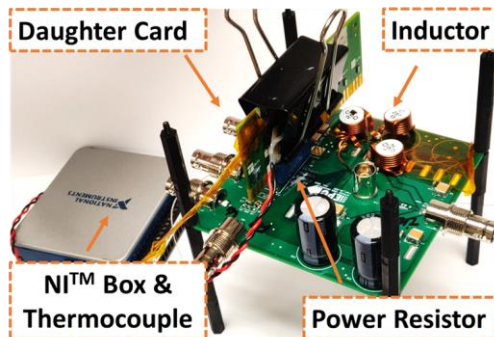
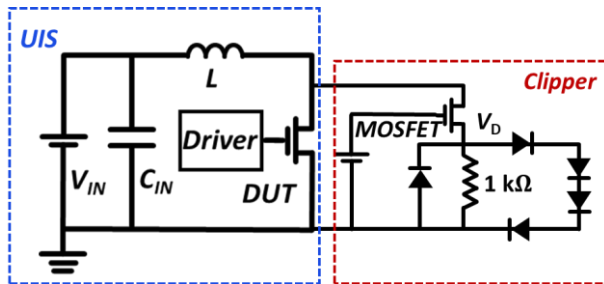
R. Zhang et al., "Overvoltage Robustness of p-Gate GaN HEMTs in High Frequency Switching up to Megahertz", IEEE Trans. Power Electron., 2023



# Device lifetime under overvoltage switching: limited by dynamic $R_{on}$

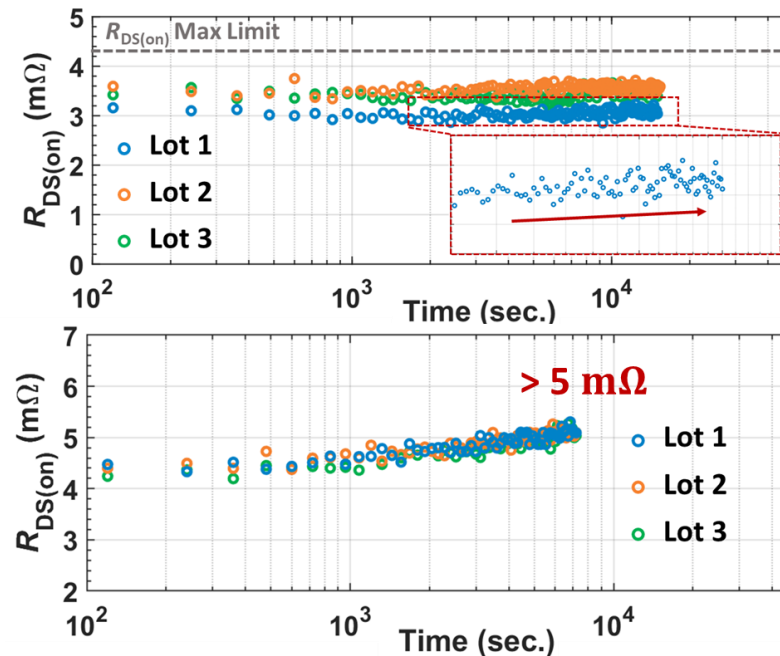
Voltage rating can be determined by long-term dynamic  $R_{ON}$  increase (e.g., 10% after 10-yr hard-switching)

## In-situ monitoring of $R_{ON}$

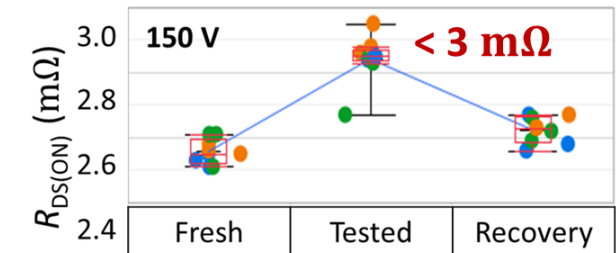


## Dynamic $R_{ON}$ increase is the major degradation in overvoltage switching

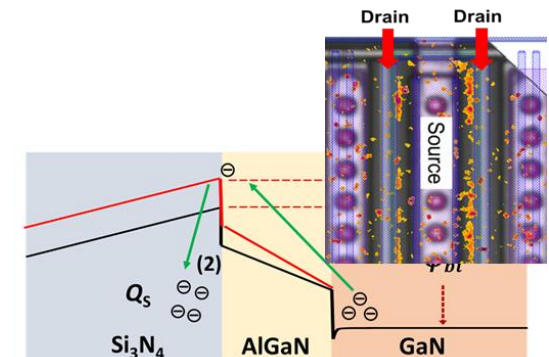
DUT: EPC2218 (100 V rated)  $f_{sw}$  : 100 kHz  
 $V_{DS}$  peak : 120 & 150 V  $T_C$  : 75 °C



## Cannot be captured by off-line measurement



## Physics-based model for lifetime projection



R. Zhang *et al.*, "In-situ RDS(on) Characterization and Lifetime Projection of GaN HEMTs Under Repetitive Overvoltage Switching," IEEE Trans. Power Electron., 2023



# Outline

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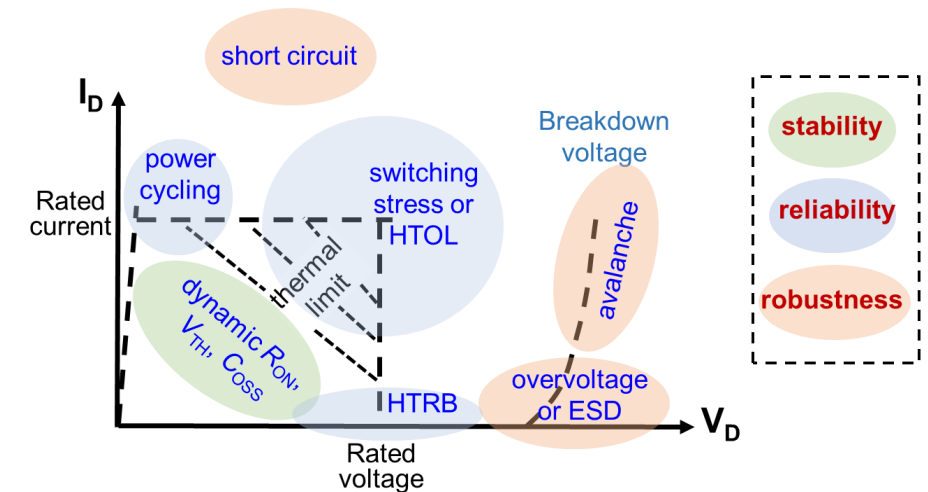
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- **Bidirectional GaN**

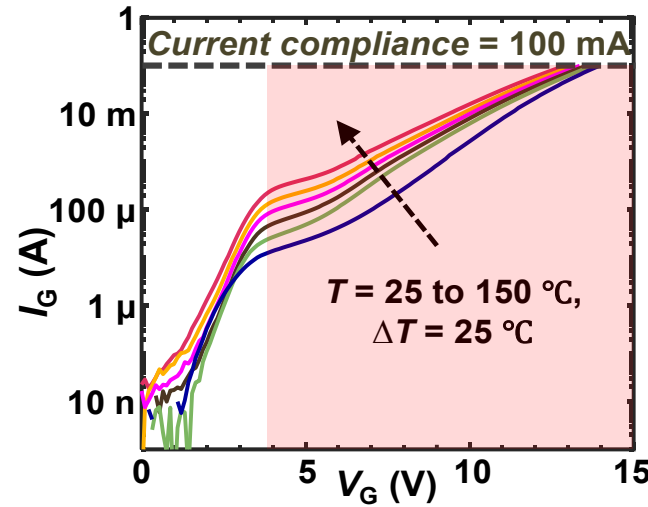
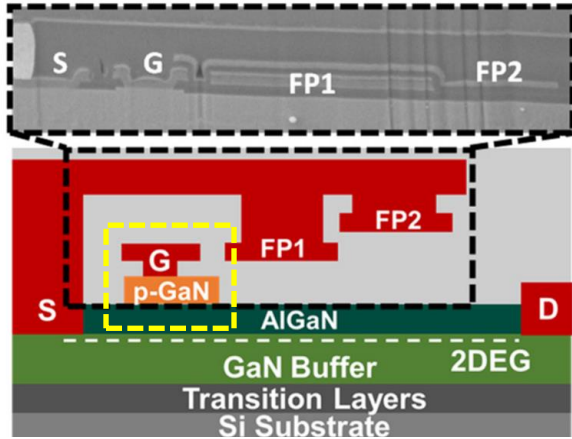
- **Vertical GaN Devices: Performance and Reliability**

- Dynamic  $R_{ON}$ , avalanche, short-circuit
- MHz converter application

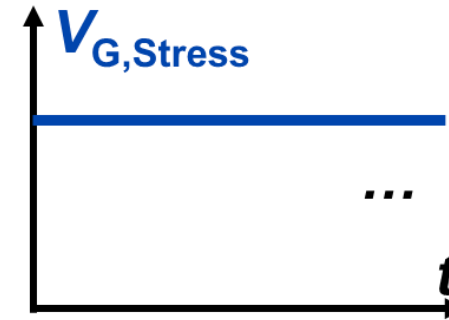
- **Summary**



# Small $V_{GS}$ headroom of p-gate GaN HEMT (as low as 1V)



## Prior methods



DC stress



Pulse-IV (AC square)

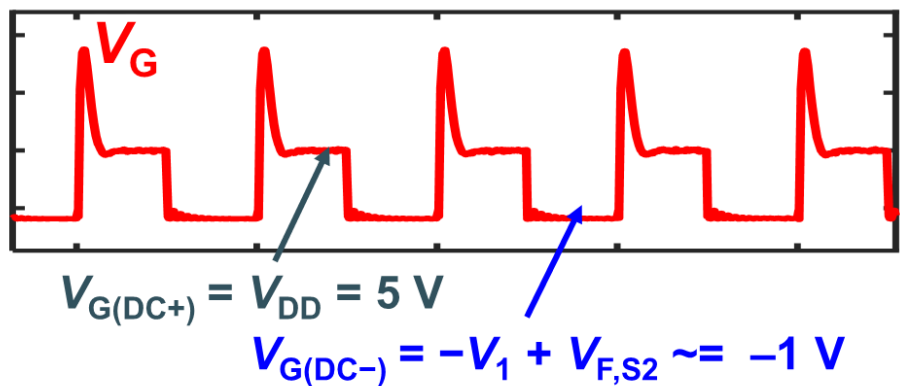
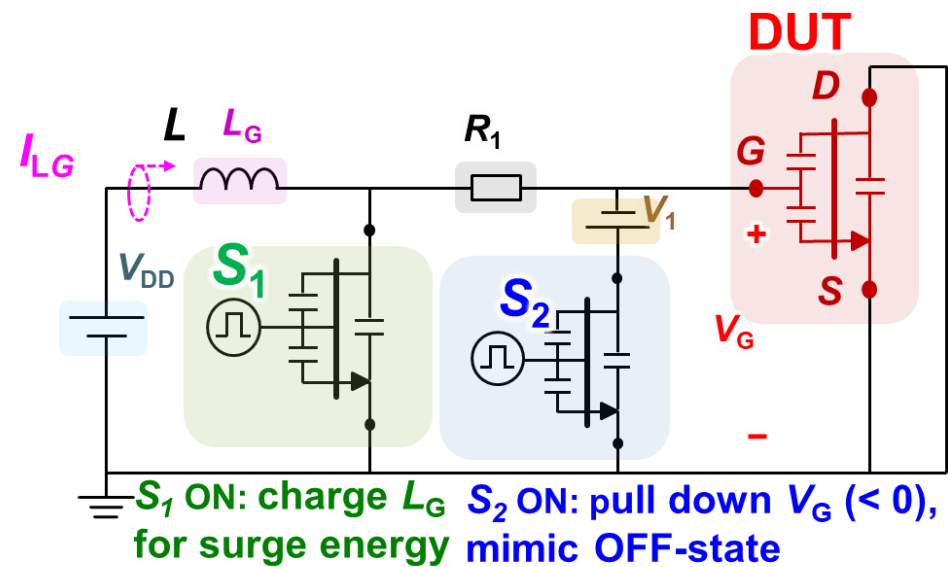
Gate-to-Source Voltage	$V_{GS}$	-10 to +7	V
Gate-to-Source Voltage - transient For $\leq 1 \mu s$	$V_{GS(transient)}$	-20 to +10	V



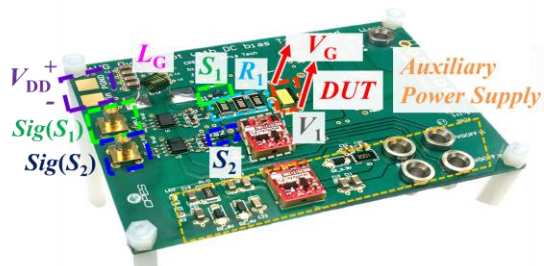
- Not RLC-resonant-like
- Slow turn on (low  $dV_G/dt$ )
- No power loop switching (i.e., drain-source grounded)



# Gate reliability evaluated by circuit method



Spec.	Symbol	Functionality	Typ. Value
Input DC V.	$V_{DD}$	<ul style="list-style-type: none"><li><math>V_{G(DC+)} = V_{DD}</math></li><li>Charge <math>L_G</math></li></ul>	5 V
Gate-loop inductor	$L_G$	<ul style="list-style-type: none"><li>Store surge energy</li><li>Modulate overshoot pulse width</li></ul>	50nH ~ 120nH
Fast switch	$S_1$	<ul style="list-style-type: none"><li>When ON, <math>L_G</math> charged by <math>V_{DD}</math></li></ul>	EPC8010
$S_1$ ON-time	$t_{ON,S1}$	<ul style="list-style-type: none"><li>Modulate <math>V_{G(PK)}</math> via surge energy</li></ul>	20ns ~ 100ns
Iso. DC V.	$V_1$	<ul style="list-style-type: none"><li><math>V_{G(DC-)} \sim -V_1</math></li></ul>	1 V
Fast switch	$S_2$	<ul style="list-style-type: none"><li>When ON, pull down <math>V_G (&lt; 0)</math></li></ul>	EPC8002
$S_2$ ON-time	$t_{ON,S2}$	<ul style="list-style-type: none"><li>Modulate <math>D</math> (via OFF time)</li></ul>	50ns ~ 50μs
Power resistor	$R_1$	<ul style="list-style-type: none"><li>Dissipate power of DC V.</li><li>Damp ringing</li></ul>	33 Ω



B. Wang et al. "Gate Switching Lifetime of P-Gate GaN HEMT: Circuit Characterization and Generalized Model." IEEE Trans. Power Electron., 2024





# Gate switching lifetime model (arbitrary $V_G$ waveform, $T$ , $f_{sw}$ )

- Voltage Acceleration Function:**

$$\sum stress^V = \int_0^T [V_G(t) - V_{G,Th}]^b dt \times \#SCTF$$

- $f_{sw}$  Acceleration Function:**

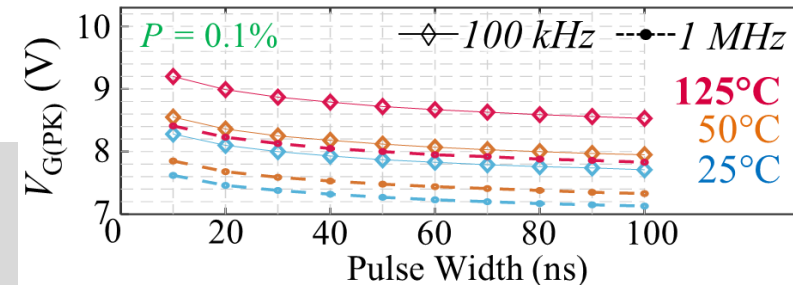
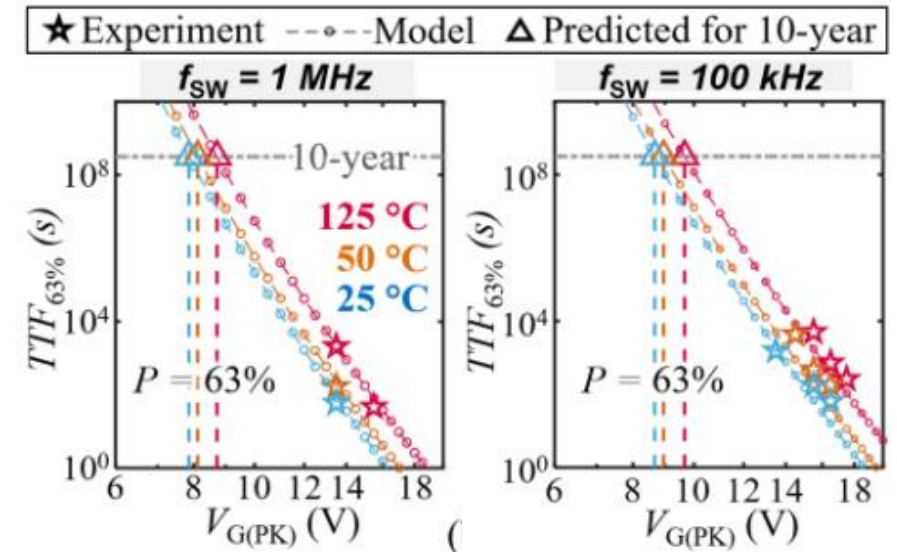
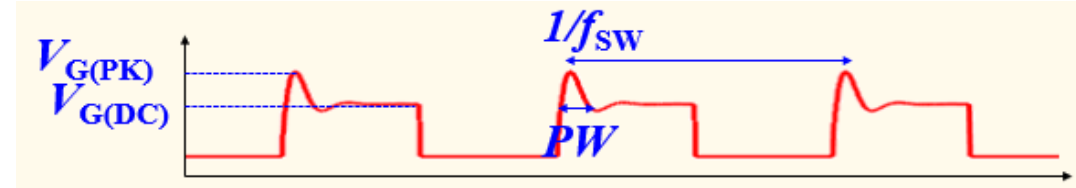
$$AF^{f_{sw}} = \begin{cases} 1 & (f_{sw} \leq f_{Th}) \\ d \cdot f_{sw}^e & (f_{Th} < f_{sw} < f_{sat}) \\ d \cdot f_{sat}^e & (f_{sw} > f_{sat}) \end{cases} \quad (e = 0.6)$$

- $T$  Acceleration Function:**

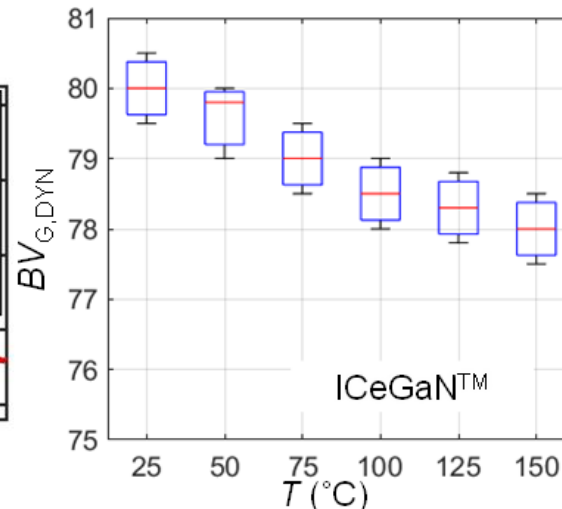
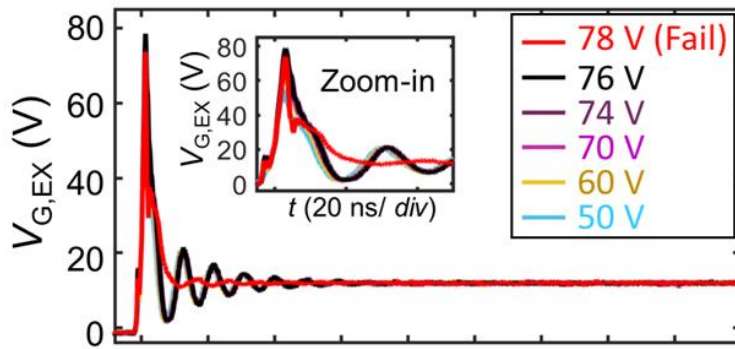
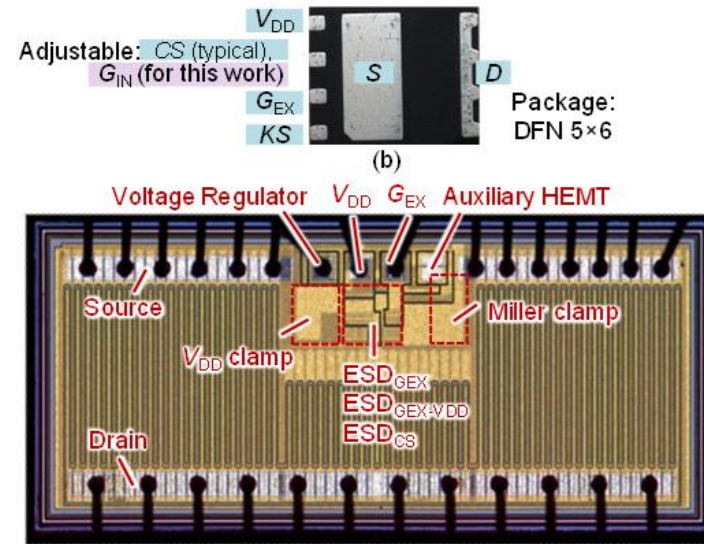
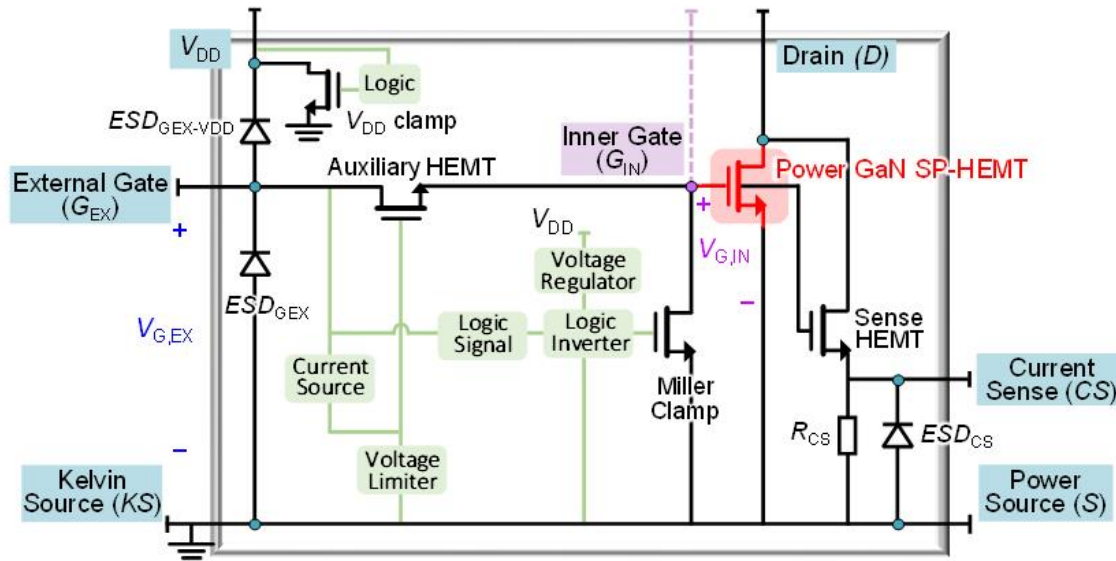
$$AF^T = \exp\left(-\frac{E_A}{kT}\right) \quad (E_A \sim -0.3 \text{ eV})$$

- Full switching model:**

$$TTF = \frac{\#SCTF}{f_{sw}} = \frac{Const.}{\int_0^T [V_G(t) - V_{G,Th}]^{2.6} dt \times f_{sw} \times AF^{f_{sw}} \times \exp\left(\frac{0.3eV}{kT}\right)}$$



# Gate robustness improvement by monolithic IC



DUT	25 °C	150 °C
ICeGaN™	80 V	78 V
Si IGBT	80 V	80 V
SiC MOSFET	70 V	70 V
Discrete GaN SP-HEMT	24 V	25 V

- ICeGaN: GaN HEMT + monolithic gate protection IC
- Gate drive voltage similar to Si IGBT and SiC MOSFET
- Fast IC response in nanosecond voltage overshoot in the gate driver loop
- Dynamic gate breakdown voltage reaches 80 V
- Rated gate voltage for continuous switching over 30 V

# Outline

- **Lateral GaN HEMT Reliability**

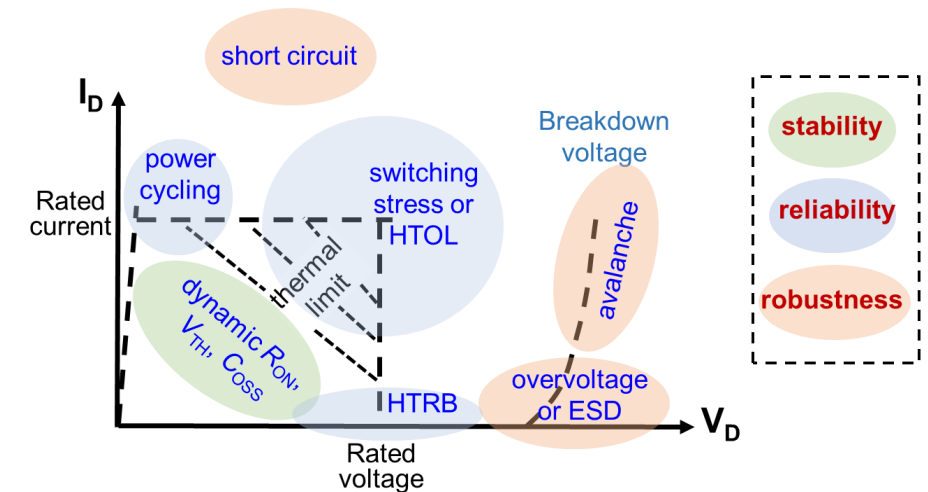
- Output capacitance loss
- Overvoltage robustness and lifetime
- Gate reliability and lifetime

- **Bidirectional GaN**

- **Vertical GaN Devices: Performance and Reliability**

- Dynamic  $R_{ON}$ , avalanche, short-circuit
- MHz converter application

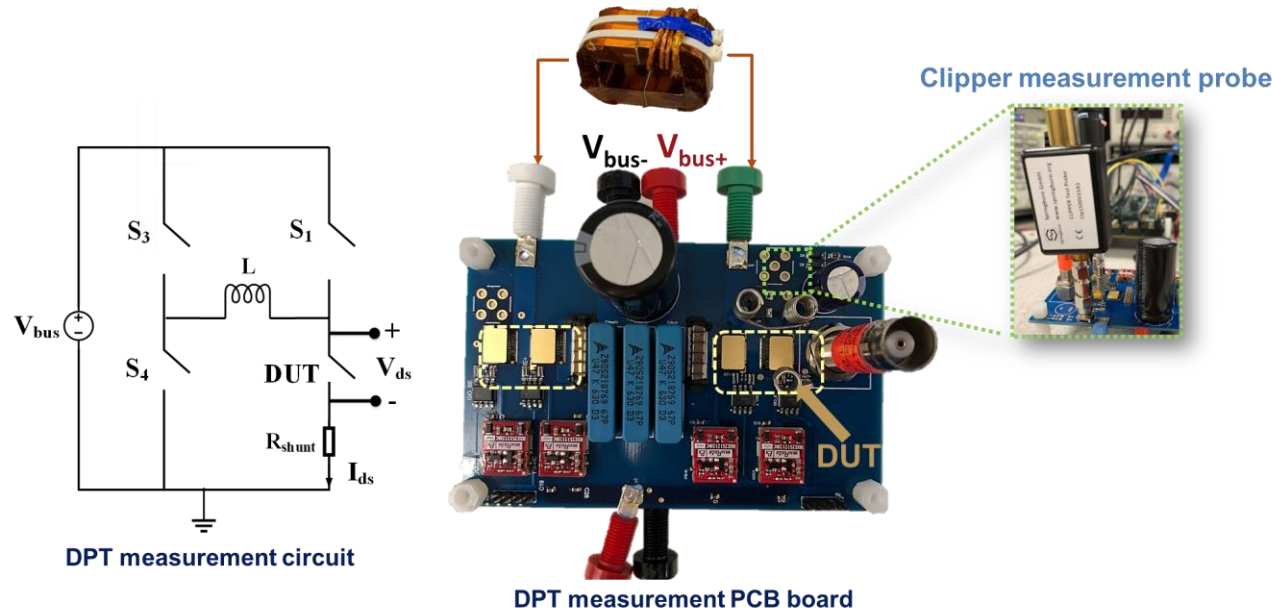
- **Summary**



# GaN Bidirectional Switch

## Dynamic $R_{ON}$ Evaluation Board for GaN BDS

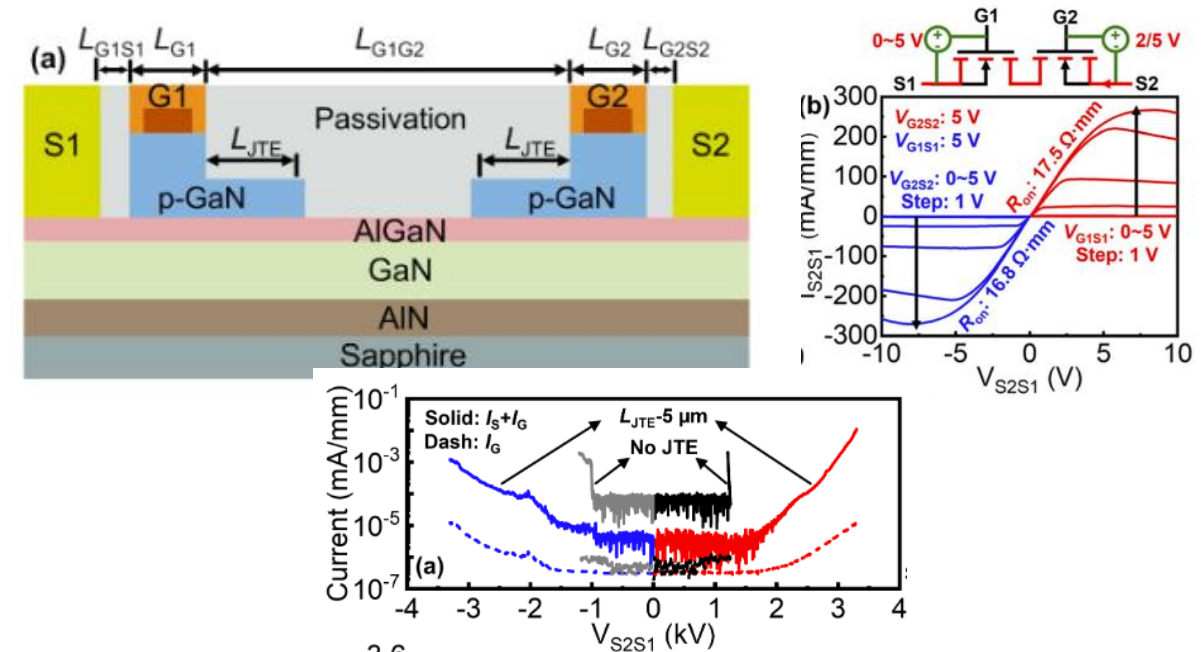
- Evaluation of industrial bidirectional GaN HEMT with and without substrate bias management
- In-situ dynamic  $R_{on}$  and  $V_{th}$  evaluation circuits for bidirectional device in hard- and soft-switching



Q. Song *et al.*, APEC 2025, best presentation award

## GaN BDS with Breakdown Voltage $> 3$ kV

- GaN BDS with BV over 3.3 kV in both polarities
- Dual p-GaN JTE, E-mode,  $R_{on,sp}$  of  $5.6 \text{ m}\Omega\cdot\text{cm}^2$
- The highest BV and best FOMs in GaN and SiC MBDS

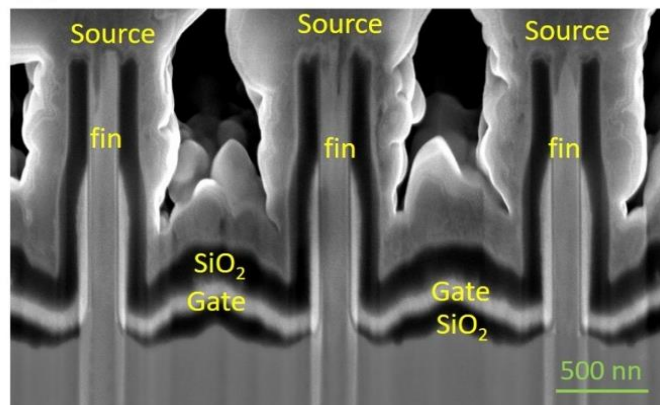
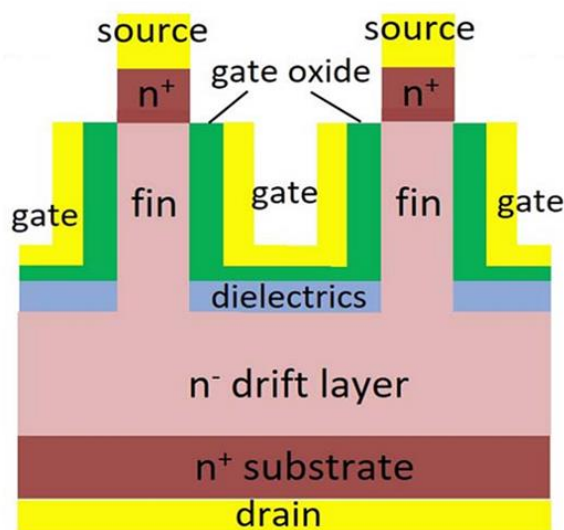


Y. Guo *et al.*, "Enhancement-Mode GaN Monolithic Bidirectional Switch With Breakdown Voltage Over 3.3 kV," EDL 2025



# Vertical GaN FinFET: from concept to commercialization

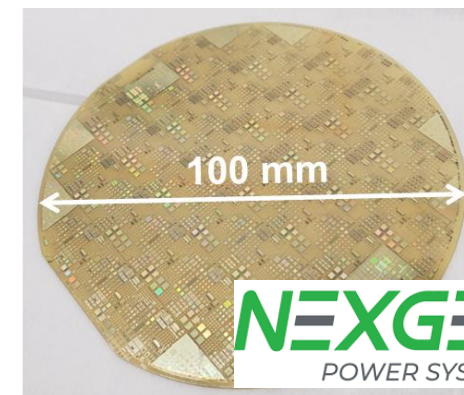
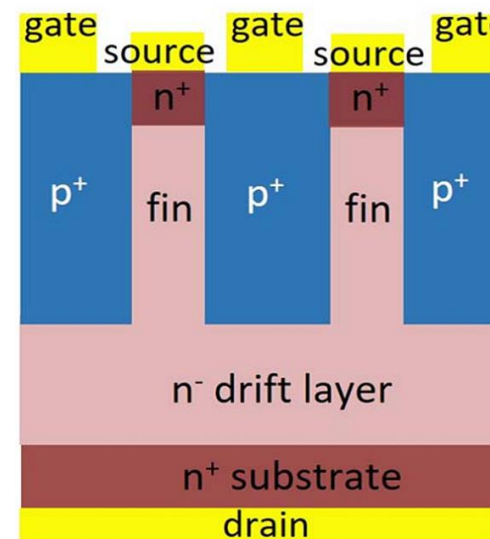
- 1.2 kV Fin-MOSFET with 200nm-wide fins
- $V_{th} \sim 1$  V;  $R_{on,sp} = 1$  m $\Omega$ ·cm<sup>2</sup>
- 2-inch GaN-on-GaN wafer process
- Superior  $R_{ON}(Q_{OSS}+Q_{rr})$  than SiC



Y. Zhang *et al.*, **IEDM** 2017

Y. Zhang *et al.*, 40 (1), **EDL**, 2019  
(2019 IEEE EDS George Smith Award)

- NexGen's 1.2 kV Fin-JFET commercialization (VT characterization & application)
- \$100M+ GaN-on-GaN Fab in Syracuse, NY
- 1470 V  $BV_{AVA}$ , avalanche capability, 0.82 m $\Omega$ ·cm<sup>2</sup> (4-5x lower than 1.2 kV SiC MOS)

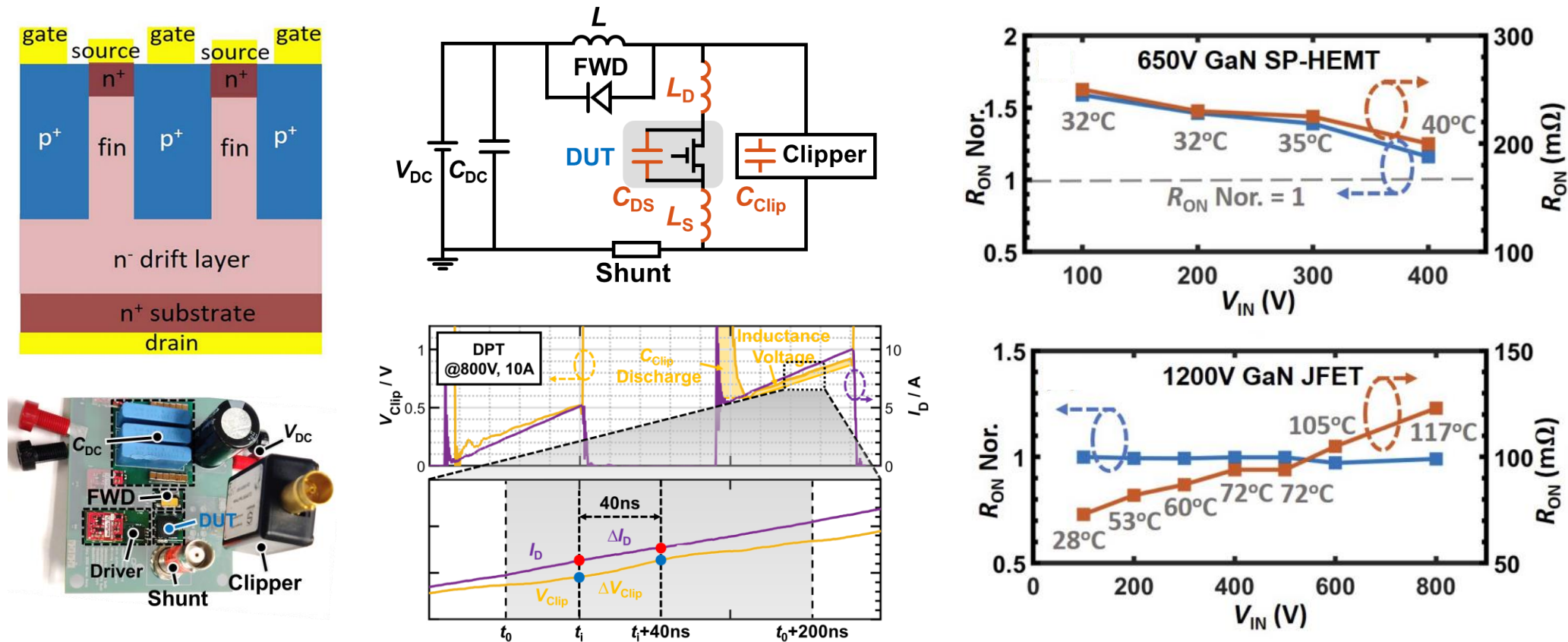


J. Liu *et al.*, **IEDM**, 23.2, 2020;  
**T-ED**, 68, 2025, 2021



# GaN devices can be dynamic $R_{ON}$ free

- Vertical GaN JFET are dynamic  $R_{ON}$  free under various voltage, current, temperature conditions
- Physics: 1) low dislocation density of GaN-on-GaN; 2) the absence of electric field crowding near the surface; 3) the minimal charge trapping in the native junction gate.

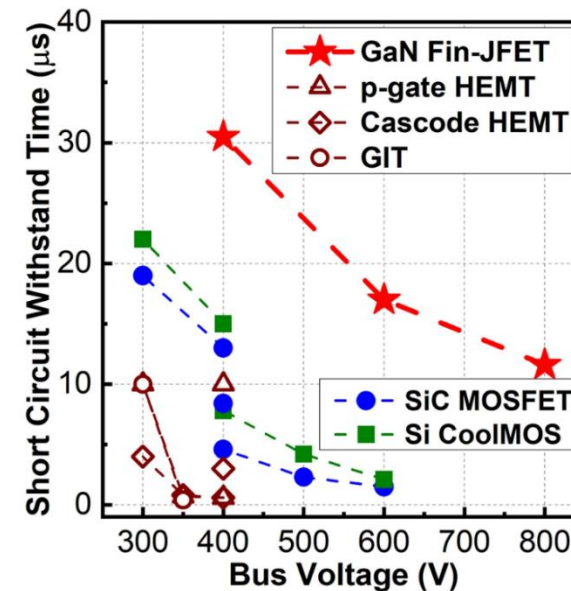
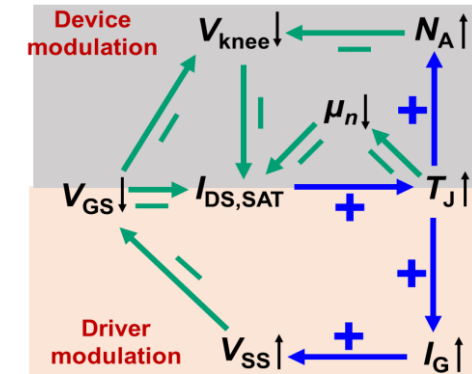
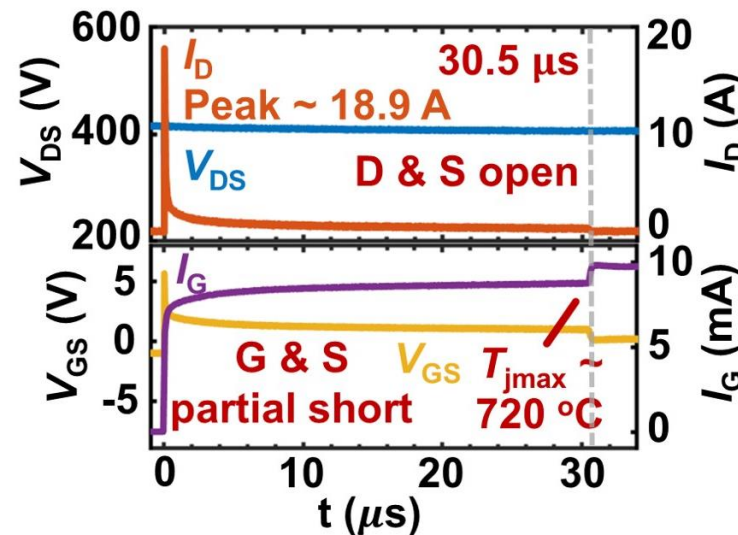
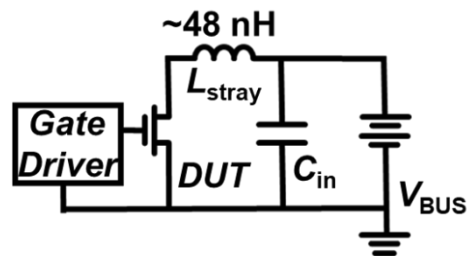
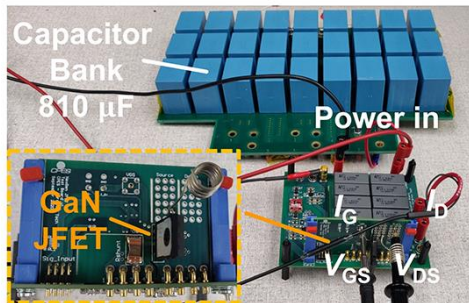


**NEXGEN**  
POWER SYSTEMS

X. Yang *et al.*, "Dynamic  $R_{ON}$  Free 1.2 kV Vertical GaN JFET," IEEE Trans. Electron. Dev., 2023

# GaN devices can achieve breakthrough short-circuit robustness

- 650V GaN JFET: 30.5  $\mu\text{s}$  @ 400 V, 10.6  $\mu\text{s}$  @ 800 V ( $BV_{AVA}$ )
- 1200V GaN JFET: >40  $\mu\text{s}$  @ 800 V
- Physics: device-driver circuit interplay to suppress  $I_{SAT}$  at high temp



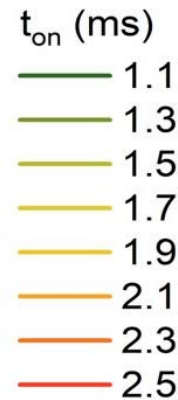
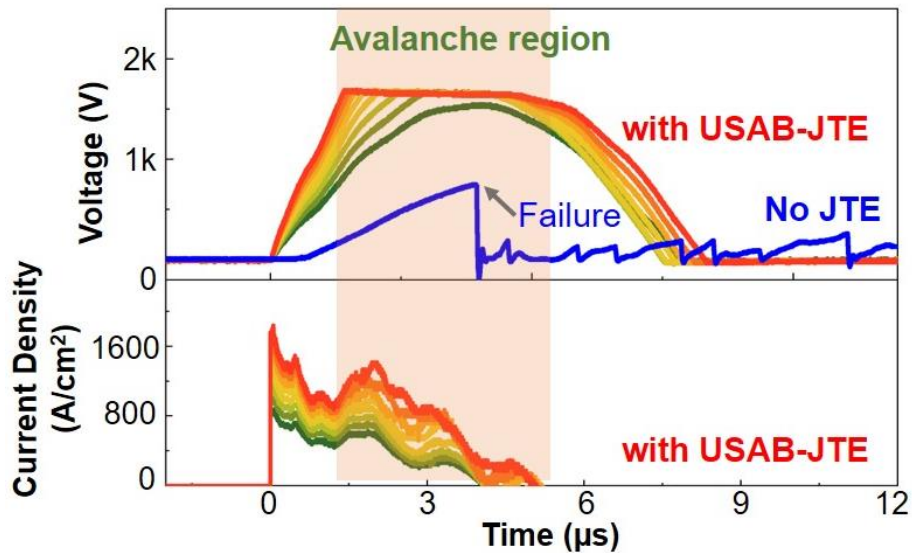
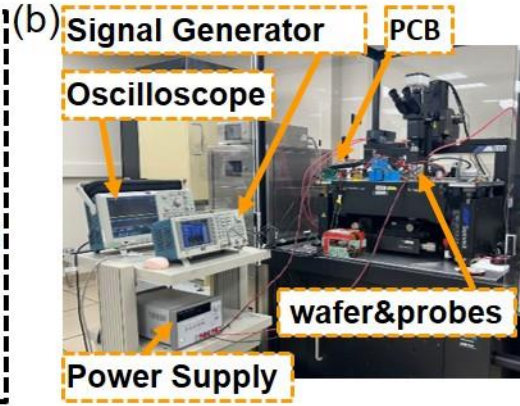
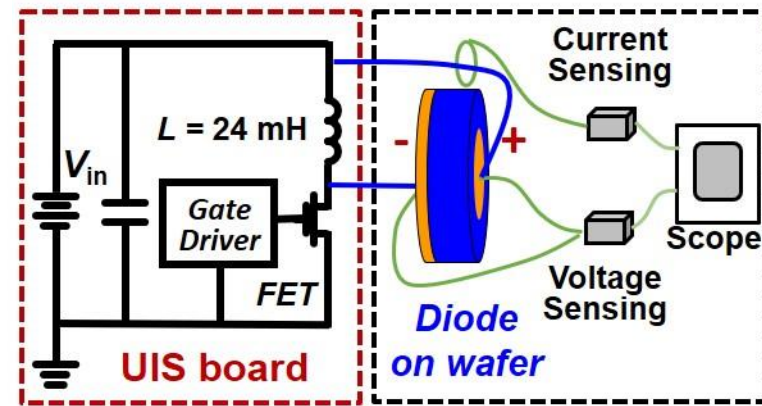
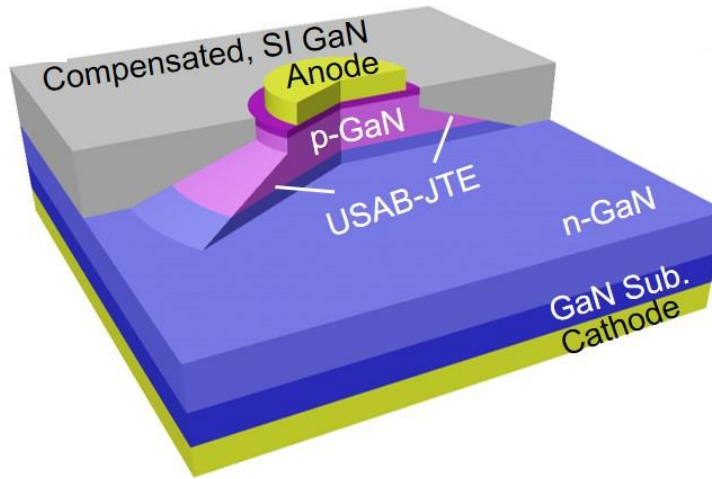
**NEXGEN**  
POWER SYSTEMS

R. Zhang *et al.*, "Breakthrough short circuit robustness demonstrated in vertical GaN fin JFET," IEEE Trans. Power Electron. 2022

X. Yang *et al.*, "Evaluation and MHz Converter Application of 1.2-kV Vertical GaN JFET," IEEE Trans. Power Electron. 2024



# GaN devices can have strong avalanche with right edge termination



- True avalanche (high  $I_{AVA}$  @  $BV_{AVA}$ ) needs to be validated by avalanche circuit test
- Small-angle beveled JTE
- Fabricated by a single implantation into p-GaN using beveled PR or dielectric mask



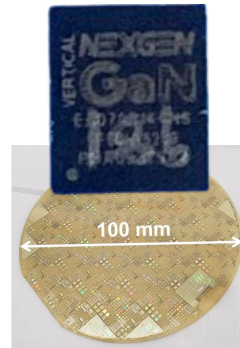
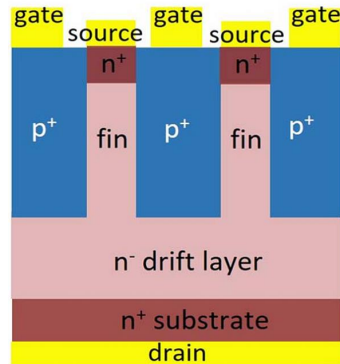
M. Xiao *et al.*, "Robust avalanche in 1.7 kV vertical GaN diodes with a single-implant bevel edge termination," EDL, (IEEE George Smith Award 2023)



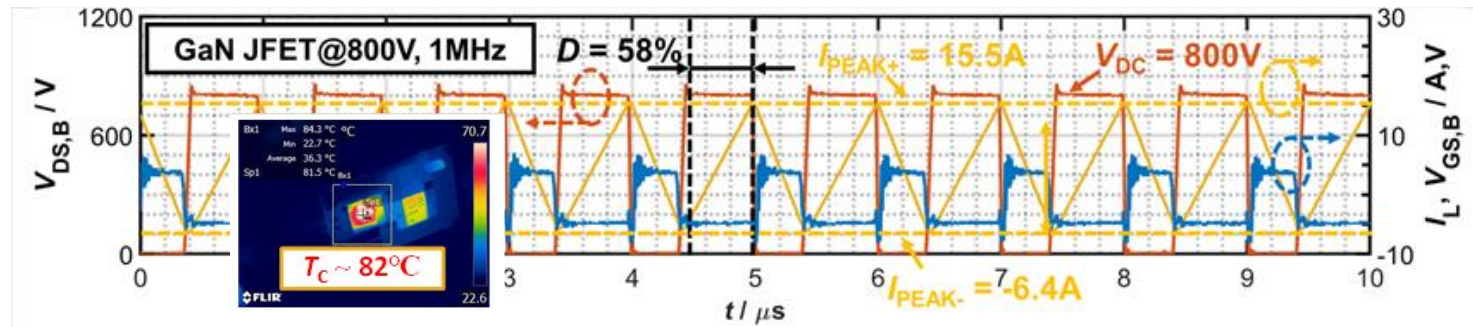


# GaN power FinFET enables kilovolt, MHz applications

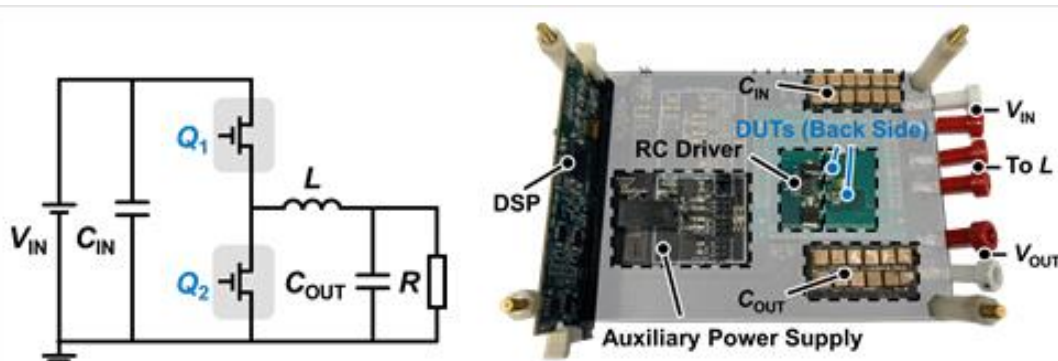
## 1.2kV, 70mΩ GaN FinFET in DFN package



## 800V, 1MHz switching with wide $D$ range



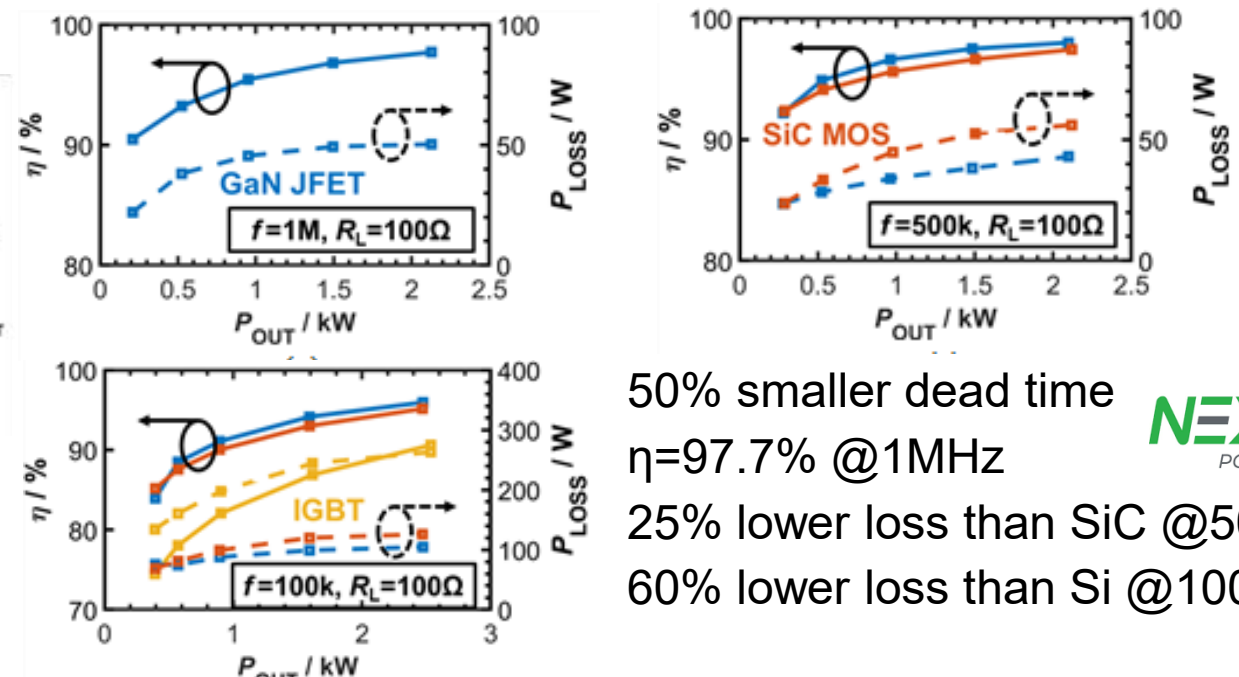
## Zero-voltage-switching buck converter



- turn-on loss  $\gg$  turn-off loss
- zero dynamic  $R_{ON}$

X. Yang *et al.*, "Evaluation and MHz Converter Application of 1.2-kV Vertical GaN JFET," **T-PEL** 2024

## Higher $f$ and efficiency than SiC and Si FETs



50% smaller dead time

$\eta = 97.7\%$  @ 1MHz

25% lower loss than SiC @ 500kHz

60% lower loss than Si @ 100kHz

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# Summary

- GaN reliability has to be evaluated in-situ under switching conditions
- Lateral GaN HEMT
  - Dynamic  $R_{ON}$  and  $C_{OSS}$  loss
    - Different trapping origins (time constants); both can be suppressed by device engineering
  - Overvoltage and surge-energy ruggedness
    - $BV$  is dynamic; dynamic  $R_{ON}$  could be the true limiter for overvoltage lifetime
  - Gate reliability and switching lifetime
    - New circuit method + switching lifetime model: arbitrary  $V_G$  waveform,  $T$  and  $f_{SW}$  dependence
- GaN monolithic bidirectional switch: new mission profiles and reliability issues
- Vertical GaN JFET
  - Dynamic  $R_{ON}$  free, better FOM than SiC MOS, robust avalanche and short-circuit

